

## HEAT - TECHNICAL CALCULATION OF THE SOLAR COLLECTOR

*Mullaev Ikromjon Israiljonovich*

*Fergana Polytechnic Institute, ikromjonmullayev83@gmail.com*

### Annotation

*this article shows how to determine the heat-technical calculation of a solar collector.*

### ARTICLE INFO

#### Article history:

Received 16 Oct 2022

Revised form 15 Nov 2022

Accepted 17 Dec 2022

© 2019 Hosting by Central Asian Studies. All rights reserved.

**Keywords:** solar collector, channel, heat flow, heat balance, heat transfer coefficient, temperature, heat losses.

\*\*\*

A flow-through solar collector is a system in which water flows through parallel channels and cools the surface of solar panels. (Fig. 1, a)

The main elements of the flat flow solar collector are as follows: the housing containing the light-absorbing panel (absorber) 1, transparent panel 2, opaque thermal insulation. The total heat flow coming to the heat carrier is determined from the heat balance:

$$Q = Q_{swal} - Q_{waste} \quad (1)$$

here:  $Q_{swal}$ ,  $Q_{waste}$  – absorbed heat flow and collector heat losses, respectively.

The solar radiation flux absorbed by the receiving panel roof consists of the direct flux, the return flux and the reverse flux:

$$Q_{swal} = \eta_0 S_n E \quad (2)$$

$$\eta_0 = \tau_{ct}(1 - \rho_n)(1 + (1 - \tau_{ct})\rho_n) \quad (3)$$

here:  $\eta_0$  – optical UWC;  $S_n$  – the surface of the illuminated surface,  $m^2$ ;  $E$  – solar flux density,  $Bt/m^2$ ;  $\tau_{ct}$  – the light transmission coefficient of the transparent panel (0,8 – 0,9);  $\rho_n$  – the reflection coefficient of the heat-absorbing panel.

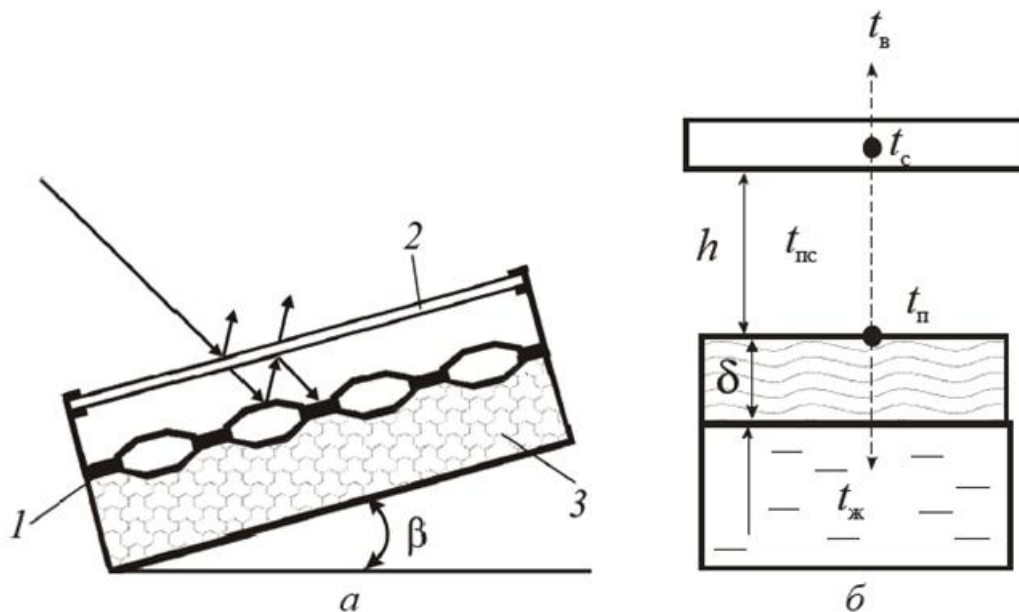
The temperature of the light-receiving surface during light absorption  $t_n$  (Fig. 1, b) increases. When the temperature of the light-absorbing panel exceeds the ambient temperature,  $t_b$  heat loss occurs:

$$Q_{nc} = K_{nc}(t_n - t_b) S_n; \quad (4)$$

$$K_{nc} = \left( \frac{1}{\alpha_{nc}^k + \alpha_{nc}^p} + \frac{\delta_{ct}}{\lambda_{ct}} + \frac{1}{\alpha_B^k + \alpha_B^p} \right) \quad (5)$$

here:  $K_{nc}$  – effective coefficient of heat loss of the solar collector  $Bt/(m^2K)$ ;  $\alpha_{nc}^k$ ,  $\alpha_{nc}^p$  – convective heat transfer and radiant heat transfer coefficients between two inclined parallel (absorbing and transparent) panels  $Bt/(m^2K)$ ;  $\delta_{ct}$ ,  $\lambda_{ct}$  – the thickness of the transparent surface and the heat transfer coefficient;

$\alpha_B^k$   $\alpha_B^p$  - coefficients of heat transfer from the transparent panel to the environment by convection and radiation,  $\text{Вт}/(\text{м}^2\text{К})$ .



1 – picture. Solar collector design and distribution of sunlight (a) and heat flow (b).

1 – light absorbing panel; 2 – mirror; 3 – thermal insulation.

Heat losses from the top absorbing surface of the collector depend on radiation and convection between the absorbing and transparent plates. Energy loss, temperature of the glass cover through convection to the environment  $t_n$  the temperature of the plate  $t_c$  is equal to the amount of energy transferred to the glass coating:

$$\alpha_{nc}^k = \frac{\lambda}{h} (0,060 - 0,00019\beta) G_r^{0,333} \quad (6)$$

here:  $\beta$  – angle of inclination of the collector relative to the horizon, grad;

$G_r = \frac{1}{(273+t_{nc})g\Delta t h^3} \nu_{nc}^2$  - Grashoff number;  $t_{nc} = (t_n + t_c)/2$  – the average temperature of the medium in the channel between the absorbing and transparent panels;  $^{\circ}\text{C}$ ;  $h$  – distance between panels, m;  $\nu_{nc}$  - of the environment  $t_{nc}$  coefficient of kinematic viscosity at temperature,  $\text{м}^2/\text{с}$ ;  $t_{nc} = (t_n - t_c)$  – difference in average temperatures of absorbent and transparent panels,  $^{\circ}\text{C}$ .

If we take into account the dependence of thermal-physical properties of air on temperature, formula 6 becomes simpler:

$$\alpha_{nc}^k = (0,060 - 0,00019\beta)(14,065 - 0,0248t_{nc})\Delta t^{0,333} \quad (7)$$

Temperature  $t_n$  from the plate, the temperature  $t_c$  the radiation coefficient of heat transfer to the glass coating is determined from the following equation:

$$\alpha_{nc}^p = \frac{G}{(t_n - t_c)(\frac{1}{\varepsilon_n} + \frac{1}{\varepsilon_c} - 1)} \left[ \left( \frac{T_n}{100} \right)^4 - \left( \frac{T_c}{100} \right)^4 \right] \quad (8)$$

here:  $\varepsilon_n$  and  $\varepsilon_c$  – the degree of blackness of the plate and glass coating, respectively.

The coefficient of heat transfer in forced convection from a transparent surface to the environment is determined from the following formula:

$$\alpha_B^k = 5,7 + 3,8v \quad (9)$$

here:  $v$  – the velocity of the outside air that washes the solar collector, m/s.

Free convection heat transfer coefficient from a transparent surface to the environment:

$$\alpha_B^k = (2,26 - 0,0067\beta)(t_c - t_B)^{0,33} \quad (10)$$

Temperature  $t_c$  is the radiation coefficient of heat transfer of the glass coating, temperature  $t_B$  takes into account the heat exchange with the air. In that case, the radiation heat transfer coefficient is as follows:

$$\alpha_B^p = \frac{G\varepsilon_c}{(t_c - t_B)} \left[ \left( \frac{T_c}{100} \right)^4 - \left( \frac{T_B}{100} \right)^4 \right] \quad (11)$$

The useful heat flow entering the heat carrier is determined by the heat transfer equation:

$$Q = k(t_n - t_{\text{ж}})S'_n \quad (12)$$

here:  $k$  – coefficient of heat transfer from the outer surface of the absorbing panel to the heat carrier,  $Wt/m^2\text{°C}$ ;  $t_{\text{ж}} = (t_{\text{ж}1} + t_{\text{ж}2})/2$  – the average temperature of the heat carrier,  $\text{°C}$ ;  $t_{\text{ж}1}$ ,  $t_{\text{ж}2}$  – the temperature of the liquid entering and leaving the collector,  $\text{°C}$ ;  $S'_p$  – the surface of the inner surface of the absorbent panel,  $m^2$ .

Heat transfer coefficient for laminar flow from absorber panel to heat carrier:

$$\alpha_{\Pi} = \frac{\lambda_{\text{ж}}}{d_{\text{ЭКВ}}} 0,15 Re_{\text{ж}}^{0,33} Pr_{\text{ж}}^{0,43} \left( \frac{Pr_{\text{ж}}}{Pr_{\Pi}} \right)^{0,25} \quad (13)$$

here:  $\lambda_{\text{ж}}$  – heat transfer coefficient of the heat carrier,  $Wt/mK$ ;  $d_{\text{ЭКВ}}$  – equivalent diameter of the heat transfer channel,  $m$ ;  $Re_{\text{ж}} = \frac{d_{\text{ЭКВ}} V_{\text{ж}}}{\nu_{\text{ж}}}$  – Reynolds number;  $Pr_{\text{ж}}$ ,  $Pr_{\Pi}$  – Prandtl number of the heat carrier, of the heat carrier  $t_{\text{ж}}$  and plate  $t_n$  determined by the average temperature;  $V_{\text{ж}}$  – average temperature velocity of the fluid in the channel  $m/s$ ;  $\nu_{\text{ж}}$  – coefficient of kinematic viscosity of the heat carrier,  $m^2/s$ .

Useful heat flow  $Q$  can also be determined by the heat absorbed by the heat carrier. In heating the flowing heat:

$$Q = GC_{\text{ж}}(t_{\text{ж}2} - t_{\text{ж}1}) \quad (14)$$

here:  $G$  – flowing fluid consumption,  $kg/s$ ;  $C_{\text{ж}}$  – specific heat capacity of the heat carrier,  $J/kg\text{°C}$ .

The maximum temperature of the heat carrier in the collector  $Q_{\text{юТ}} = Q_{\text{иС}}$  determined by the condition.

$$\text{In that case } \eta_0 S_n E = (t_{\text{мex}} - t_B) K_{\text{иС}}^{\text{mex}} S_n$$

In this case, the maximum temperature of the heat carrier,  $\text{°C}$ :  $t_{\text{мex}} = \frac{\eta_0 E}{K_{\text{иС}}^{\text{mex}}} + t_B$

Solar collector U.W.C. is determined from the following formula:

$$\eta = \frac{Q}{S_n E} = \eta_0 - K_{\text{иС}} \frac{t_n - t_B}{E}$$

here:  $\eta_0$  – optical U.W.C., (0,78 – 0,85);  $K_{\text{иС}}$  – coefficient of heat loss,  $BT/m^2\text{°C}$ .

Description of the solar collector -  $\eta$  of  $\frac{t_n - t_B}{E}$  dependence on is determined during its testing.

Effective optics for a south-facing single-glazed solar collector U.W.C.  $\eta_3 = 0,95\eta_0$  and for double glazing  $\eta_3 = 0,93\eta_0$

Solar energy flux density  $E$  is less than the critical value, the solar collector's U.W.C. will be zero:

$$E_{\text{кр}} = \frac{K_{\text{иС}}}{\eta_0} (t_{\text{ж}1} - t_B) \quad (16)$$

The average U.W.C of the solar collector for a certain period of time (day, month, year):

$$\eta_{\text{ѳпТ}} = \frac{\Sigma(\eta E)}{E_{\text{ѳпТ}}} \quad (17)$$

Sum only  $E > E_{кр}$  is calculated for time intervals,  $Вт/м^2$ .

The effectiveness of the absorbent surface is determined by its construction. If we take into account that the absorbing panel performs two tasks: it absorbs sunlight and transfers heat to the heat carrier, then the design of the absorbing panel depends on the coefficient of heat loss  $K_{ис}$  and affects the coefficient of heat transfer from the panel to the heat carrier. However, the method of calculating heat losses for the constructions of absorbing panels is not fundamentally different - only  $K$ ,  $S_n$ ,  $S'_n$ ,  $A$ ,  $d_{эКВ}$  it is necessary to express the parameters correctly and use the formulas given above.

## Literature

1. Abbasov, E. S. (2004). Calculation of the turbulized boundary layer in diffusor-confusor solar receivers. *Applied Solar Energy*, 40(1), 92-94.
2. Abbasov, E. S. (2004). Heat exchange intensification in solar heat collectors of solar air heaters. *Applied solar energy*, 39(4), 20-23.
3. Mamatisaev, G., & Muulayev, I. (2022). ECOLOGICAL AND TECHNOLOGICAL PROBLEMS IN WATER COLLECTION FACILITIES. *Science and innovation*, 1(A7), 767-772.
4. Mullaev, I. (2022). ҚУЁШ-ҲАВО ИСИТИШ ҚУРИЛМАСИНИНГ САМАРАДОРЛИГИНИ ОШИРИШ. *Science and innovation*, 1(A7), 756-761.
5. Abobakirovich, Abdulkarimov Bekzod, Abbasov Yorgin Sodikovich, and Mullaev Ikromjon Isroiljon Ogli. "Optimization of operating parameters of flat solar air heaters." *Вестник науки и образования* 19-2 (73) (2019): 6-9.
6. Madaliev, M. E. U., Maksudov, R. I., Mullaev, I. I., Abdullaev, B. K., & Haidarov, A. R. (2021). Investigation of the Influence of the Computational Grid for Turbulent Flow. *Middle European Scientific Bulletin*, 18, 111-118.
7. Azizovich, N. I. (2022). On The Accuracy of the Finite Element Method on the Example of Problems about Natural Oscillations. *European Multidisciplinary Journal of Modern Science*, 116-124.
8. Nasirov, I. (2022). АКТУАЛЬНОСТЬ ПРИМЕНЕНИЯ МЕТОДОВ МАТЕМАТИЧЕСКОГО МОДЕЛИРОВАНИЯ И МЕТОДОВ КОНЕЧНЫХ ЭЛЕМЕНТОВ В СТРОИТЕЛЬСТВЕ. *Science and innovation*, 1(A7), 711-716.
9. Nosirov, A. A., & Nasirov, I. A. (2022). Simulation of Spatial Own of Vibrations of Axisymmetric Structures. *European Multidisciplinary Journal of Modern Science*, 107-115.
10. Akramovna, U. N., & Ismoilovich, M. R. (2021). Flow Around a Plate at Nonzero Cavitation Numbers. *CENTRAL ASIAN JOURNAL OF THEORETICAL & APPLIED SCIENCES*, 2(12), 142-146.
11. Muminov, O., & Maksudov, R. (2022). HIDROTECHNICS PREVENT VIBRATIONS THAT OCCUR IN CONSTRUCTIONS. *Science and innovation*, 1(A7), 762-766.
12. Madaliev, E. U., & qizi Abdukhalilova, S. B. (2022). Repair of Water Networks. *CENTRAL ASIAN JOURNAL OF THEORETICAL & APPLIED SCIENCES*, 3(5), 389-394.
13. qizi Abdukhalilova, S. B. (2021). Simplified Calculation of the Number of Bimetallic Radiator Sections. *CENTRAL ASIAN JOURNAL OF THEORETICAL & APPLIED SCIENCES*, 2(12), 232-237.
14. Usmonova, N. A. (2021). Structural Characteristics of the Cavern at a Fine Bubbled Stage of Cavitation. *Middle European Scientific Bulletin*, 18, 95-101.
15. Usmanova, N., & Abdukhalilova, S. (2022). SHELL-AND-TUBE HEAT EXCHANGER DESIGN WITH INCREASED TURBULENCE OF THE HEATED LIQUID FLOW. *Science and innovation*, 1(A7), 726-731.

16. Madaliyev, E., Makhsitalayev, B., & Rustamova, K. (2022). IMPROVEMENT OF SEWAGE FLATS. *Science and innovation*, 1(A7), 796-801.
17. Madaliyev, E., & Maksitaliyev, B. (2022). A NEW WAY OF GETTING ELECTRICITY. *Science and innovation*, 1(A7), 790-795.
18. Koraboevich, U. M., & Ilhomidinovich, M. G. (2021, June). Calculation of the free vibrations of the boxed structure of large-panel buildings. In " *ONLINE-CONFERENCES*" PLATFORM (pp. 170-173).
19. Madraximov, M. M., Nurmuxammad, X., & Abdulkhaev, Z. E. (2021, November). Hydraulic Calculation Of Jet Pump Performance Improvement. In *International Conference On Multidisciplinary Research And Innovative Technologies* (Vol. 2, pp. 20-24).
20. Maqsudov, R. I., & qizi Abdukhalilova, S. B. (2021). Improving Support for the Process of the Thermal Convection Process by Installing. *Middle European Scientific Bulletin*, 18, 56-59.
21. Muminov, O. (2022). TYPES OF CAVITATION, CAUSING VIBRATION IN ENGINEERING AND WATER SUPPLY SYSTEMS. *Science and innovation*, 1(A7), 732-737.
22. Mo'minov, O. A., & O'tbosarov Sh, R. TYPE OF HEATING RADIATORS, PRINCIPLES OF OPERATION AND THEORETICAL ANALYSIS OF THEIR TECHNICAL AND ECONOMIC CHARACTERISTICS.
23. O'tbosarov, S., & Xusanov, N. (2022). ASSEMBLY OF STRUCTURES AND WATER DIVIDERS. *Science and innovation*, 1(A7), 780-784.
24. Mo'minov, O. A., Abdukarimov, B. A., & O'tbosarov, S. R. (2021). Improving support for the process of the thermal convection process by installing reflective panels in existing radiators in places and theoretical analysis. In *Наука и инновации в строительстве* (pp. 47-50).
25. Abbasov, Y., & Usmonov, M. (2022). CALCULATION OF THEIR POWER AND HEATING SURFACE IN IMPROVING THE EFFICIENCY OF AIR HEATING SYSTEMS. *Science and innovation*, 1(A7), 738-743.
26. Abbasov, Y. S., & ugli Usmonov, M. A. (2022). Design of an Effective Heating System for Residential and Public Buildings. *CENTRAL ASIAN JOURNAL OF THEORETICAL & APPLIED SCIENCES*, 3(5), 341-346.
27. Ismailov, M., & Xolmatov, I. (2022). КАНАЛИЗАЦИЯ ТАРМОҚЛАРИНИ ЛОЙИХАЛАШНИНГ АПТИМАЛ УСУЛЛАРИ. *Science and innovation*, 1(A7), 744-749.
28. Рашидов, Ю. К., Орзиматов, Ж. Т., & Исмоилов, М. М. (2019). Воздушные солнечные коллекторы: перспективы применения в условиях Узбекистана. *ББК 20.1 я43 Э 40*.
29. Ismailov, M., & Xolmatov, I. (2022). OPTIMAL METHODS FOR DESIGNING SEWER NETWORKS. *Science and Innovation*, 1(7), 744-749.
30. Ибрагимова, З. К. К., Хамдамова, Н. С. К., Умуркулов, Ш. Х. У., & Сабиров, Д. Р. У. (2022). ПОДГОТОВКА ПИТЬЕВОЙ ВОДЫ ИЗ МАЛОМОЩНЫХ ПОВЕРХНОСТНЫХ ВОДОИСТОЧНИКОВ. *Central Asian Research Journal for Interdisciplinary Studies (CARJIS)*, 2(Special Issue 4), 77-83.
31. Abdullayev, B. X., & Rahmankulov, S. A. (2021). Modeling Aeration in High Pressure Hydraulic Circulation. *CENTRAL ASIAN JOURNAL OF THEORETICAL & APPLIED SCIENCES*, 2(12), 127-136.
32. Abdullayev, B. X., & Rahmankulov, S. A. (2021). Movement of Variable Flow Flux Along the Path in a Closed Inclined Pipeline. *CENTRAL ASIAN JOURNAL OF THEORETICAL & APPLIED SCIENCES*, 2(12), 120-126.
33. Xamdaliyevich, S. A., & Rahmankulov, S. A. (2021, July). Investigation of heat transfer processes of solar water, air contact collector. In *E-Conference Globe* (pp. 161-165).



34. Husanov, N., & Abdukhalilova, S. (2022). HEAT EXCHANGE PROCESSES IN A SHELL-AND-TUBE HEAT EXCHANGER. *Science and innovation*, 1(A7), 721-725.
35. Аббасов, Ё. (2020). Роль солнечных воздухонагревателей в теплоэнергетической отрасли и перспективы их развития в Республике Узбекистан. *Общество и инновации*, 1(1), 1-13.

